

21. Maxwell's Equations

The story so far:

$$\underline{\nabla} \cdot \underline{D} = \rho_f$$

Coulomb's Law / Gauss' Law

$$\underline{\nabla} \wedge \underline{E} = -\partial \underline{B} / \partial t$$

Faraday's Law of induction

$$\underline{\nabla} \cdot \underline{B} = 0$$

No magnetic monopoles (from Ampère's law)

$$\underline{\nabla} \wedge \underline{H} = \underline{J}_f$$

Ampère's Law

As you probably know, this is not the final form of Maxwell's equations.

$$\underline{\nabla} \cdot (\underline{\nabla} \wedge \underline{H}) = \underline{\nabla} \cdot \underline{J}_f = 0 \quad (\text{div curl of any vector is } \underline{\text{zero}})$$

but equation of continuity $\underline{\nabla} \cdot \underline{J}_f + \frac{\partial \rho_f}{\partial t} = 0$
(charge conservation)

Thus, unless $\partial \rho_f / \partial t = 0$ there is something wrong with the fourth equation, above.

The "fix" - due to Maxwell - is the introduction of the displacement current $\underline{J}_d \Rightarrow \underline{\nabla} \wedge \underline{H} = \underline{J}_f + \underline{J}_d$

then

$$\underline{\nabla} \cdot \underline{\nabla} \wedge \underline{H} = 0 = \underline{\nabla} \cdot \underline{J}_f + \underline{\nabla} \cdot \underline{J}_d = -\frac{\partial \rho_f}{\partial t} + \underline{\nabla} \cdot \underline{J}_d$$

$$\Rightarrow \underline{\nabla} \cdot \underline{J}_d - \frac{\partial}{\partial t} (\underline{\nabla} \cdot \underline{D}) = 0$$

$$\text{or } \nabla \cdot (\underline{J}_d - \frac{\partial \underline{D}}{\partial t}) = 0$$

$$\underline{J}_d = \frac{\partial \underline{D}}{\partial t} \quad \text{displacement current} \left[\begin{array}{l} \text{due to rate of change} \\ \text{of displacement vector} \end{array} \right]$$

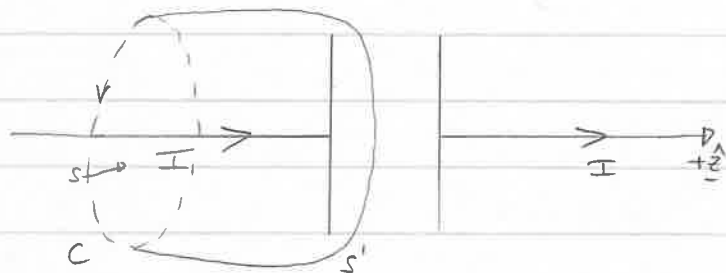
$$\text{and so } \nabla \times \underline{H} = \underline{J}_f + \frac{\partial \underline{D}}{\partial t}$$

The inclusion of the displacement current leaves the tangential boundary conditions on $\underline{H}$ (defined by $\nabla \times \underline{H}$) unchanged, but alters the integral form of Ampere's law $H_{2n} - H_{1n} = \int_C \underline{J}_f \cdot \underline{a}$

$$\oint_C \underline{H} \cdot d\underline{s} = I_{fenc} + I_{denc}$$

$$\int_S \underline{J}_f \cdot d\underline{a} + \int_S \frac{\partial \underline{D}}{\partial t} \cdot d\underline{a}$$

* Practically the need for the displacement current can be seen by examining the parallel plate capacitor [immediately following connection to a battery]



$$\text{Evaluate } \oint_C \underline{H} \cdot d\underline{s} = \int_S \underline{J}_f \cdot d\underline{a}$$

$$\text{when } S \text{ is the disk bounded by } C \quad \int_S \underline{J}_f \cdot d\underline{a} = I$$

But S can be chosen at will - provided that it is bounded by C - that is we could choose S' . In this case $\int_{S'} \underline{J}_f \cdot d\underline{a}$ is zero. But since $\underline{D} = \epsilon \underline{E} = q/A \underline{\hat{z}}$

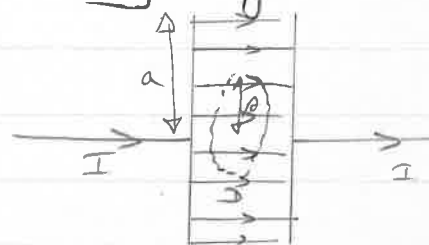
$$\underline{E} = \frac{\Delta \phi}{\underline{\hat{z}}} \quad C = \frac{q}{\Delta \phi} = \frac{A \epsilon}{d} \quad \text{or } \int_{S'} \underline{D} \cdot d\underline{a} = q$$

then $\partial \mathcal{D} / \partial t = (\partial q / \partial t) / A = I / A$

and $\int_{S'} \frac{\partial \mathcal{D}}{\partial t} \cdot d\mathbf{a} = I = \int_{S'} \mathbf{J}_a \cdot d\mathbf{a}$

and inclusion of the displacement current saves the day.
 [Note that $\mathcal{D}$ is only changing when the charge on the capacitor plates is changing (i.e. during charge or discharge (DC)). When the capacitor is no longer being charged there is neither $\mathbf{I}_f$ or $\mathbf{I}_a$]

The displacement current is distributed uniformly throughout the space occupied by the capacitor, thus when applying ampere's law around a circular loop as shown we obtain



$$\oint \mathbf{H} \cdot d\mathbf{s} = \frac{I \cdot \pi \rho^2}{\pi a^2}$$

* Application of the boundary conditions on $\mathbf{H}$ leads to a radial surface current $\mathbf{K}_f$ flowing outwards from the centre of the capacitor on each plate. [p352]
 [This is the distribution of charge during the Δt when the current is turned on]

* It must be emphasised that $\mathbf{I}_a$, is not a current of moving charges — but it does provide an alternative, equivalent, source of magnetic field $\mathbf{H}$.

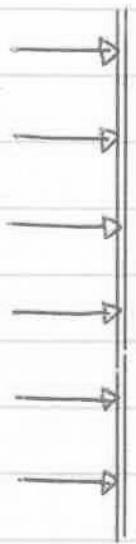
$$\nabla \wedge \mathbf{H} = \frac{\partial \mathcal{D}}{\partial t} (+ \mathbf{J}_f)$$

Can be thought of as the "magnetic" form of Faraday's Law of induction — a changing $\mathbf{E}$ ($\mathcal{D}$) gives rise to an $\mathbf{H}$ ($\mathcal{B}$) field. (Just as Faraday's Law says that a changing $\mathcal{B} \Rightarrow \mathbf{E}$)

In fact, we will see later that the displacement current term of $\nabla \times \underline{E}$ is essential to the existence of em waves.

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After inclusion of the displacement current we obtain the complete set of Maxwell's equations



$$\nabla \cdot \underline{D} = \rho_f$$

Coulomb/Gauss

$$\oint_S \underline{D} \cdot d\underline{a} = \int_V \rho_f d\tau$$

$$\nabla \times \underline{E} = -\frac{\partial \underline{B}}{\partial t}$$

Faraday

$$\oint_C \underline{E} \cdot d\underline{s} = -\int \frac{\partial \underline{B}}{\partial t} \cdot d\underline{a}$$

$$[\underline{E} = -d\Phi_B/dt]$$

$$\nabla \cdot \underline{B} = 0$$

Ampere + no mag monopoles

$$\oint_S \underline{B} \cdot d\underline{a} = \Phi_B = 0$$

[note that Φ_B not necessarily zero unless surface is closed]

$$\nabla \times \underline{H} = \underline{J}_f + \frac{\partial \underline{D}}{\partial t}$$

Ampere + Maxwell

$$\oint_C \underline{H} \cdot d\underline{s} = \int_S \underline{J}_f \cdot d\underline{a} + \int_S \frac{\partial \underline{D}}{\partial t} \cdot d\underline{a}$$

Add to these

$$\underline{D} = \epsilon_0 \underline{E} + \underline{P}$$

$$\underline{H} = \underline{B}/\mu_0 - \underline{M}$$

the Lorentz force law

$$\underline{F} = q(\underline{E} + \underline{v} \times \underline{B})$$

and the boundary conditions

$$D_{2n} - D_{1n} = \sigma_f$$

$$E_{2t} - E_{1t} = 0$$

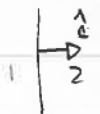
$$B_{2n} - B_{1n} = 0$$

$$H_{2t} - H_{1t} = \underline{k}_f \wedge \hat{n} \quad [\hat{n} \text{ from } 1 \rightarrow 2]$$

plus equation of continuity

$$\nabla \cdot \underline{J} + \partial \rho / \partial t = 0$$

and we have the entire classical em theory in one simple, compact, form.



* Depending on the particular circumstances it may be more convenient to write Maxwell's equations in slightly different forms e.g. $\underline{E}, \underline{B}$ (+ $\underline{P}, \underline{M}$) or for l.i.h. media in terms of just $\underline{E}, \underline{B}$ or $\underline{E}, \underline{H}$. (p 357-358) [and the problems]
 $[\underline{D} = \epsilon \underline{E}, \underline{B} = \mu \underline{H}]$ are called constitutive equations]

* Energy Flow and the Poynting Vector

$$W = \int_V \underline{J}_F \cdot \underline{E} \, d\tau = \text{rate at which em energy is converted into heat (watts)} \quad \left(\begin{array}{l} \text{See Chap 12} \\ 12-35 \end{array} \right)$$

Substituting $\underline{J}_F = \nabla \wedge \underline{H} - \partial \underline{D} / \partial t$

$$W = \int_V \underline{E} \cdot (\nabla \wedge \underline{H}) \, d\tau - \int_V (\underline{E} \cdot \partial \underline{D} / \partial t) \, d\tau$$

but

$$\underline{E} \cdot (\nabla \wedge \underline{H}) = \underline{H} \cdot (\nabla \wedge \underline{E}) - \nabla \cdot (\underline{E} \wedge \underline{H}) = -\underline{H} \cdot \partial \underline{B} / \partial t - \nabla \cdot (\underline{E} \wedge \underline{H})$$

$$\Rightarrow W = - \int_V (\underline{H} \cdot \partial \underline{B} / \partial t + \underline{E} \cdot \partial \underline{D} / \partial t) \, d\tau - \int_V \nabla \cdot (\underline{E} \wedge \underline{H}) \, d\tau$$

but for l.i.h media $\underline{H} = \underline{B} / \mu$ and $\underline{D} = \epsilon \underline{E}$

$$\Rightarrow W = - \frac{\partial}{\partial t} \int_V \underbrace{\left(\frac{1}{2} \epsilon \underline{E}^2 + \frac{1}{2\mu} \underline{B}^2 \right)}_{\text{Total em energy}} \, d\tau - \oint_S (\underline{E} \wedge \underline{H}) \cdot d\mathbf{a}$$

Poynting's Theorem

$$\Rightarrow \underbrace{- \frac{\partial}{\partial t} \int_V u_{\text{tot}} \, d\tau}_{\text{rate of decrease of em energy}} = \underbrace{W}_{\substack{\downarrow \\ \text{rate of} \\ \text{convert to heat}}} + \underbrace{\oint_S (\underline{E} \wedge \underline{H}) \cdot d\mathbf{a}}_{\substack{\downarrow \\ \text{rate of loss of} \\ \text{em energy from } V \\ \text{(rate at which energy leaves} \\ \text{ } V. \text{ If } < 0 \text{ then energy is} \\ \text{flowing into volume)}}$$

$u_{\text{tot}} = u_e + u_m$

$\underline{E} \wedge \underline{H} = \underline{S}$ — Poynting vector (power flux)
 energy current density, "points" in the
 direction of energy flow.
 Watts/m² (intensity)

Problems : Chap 21 — 1, 3, 7, 9, 12

↓
 linear non-homogeneous

$$\Rightarrow \epsilon(\underline{r}) \quad \mu(\underline{r})$$

$$\underline{E} = \underline{D} \quad \underline{B} = \mu(\underline{r}) \underline{H}$$